OPERATING INSTRUCTIONS

TYPE 1001-A

STANDARD-SIGNAL GENERATOR

1001-A

GENERAL RADIO COMPANY

L

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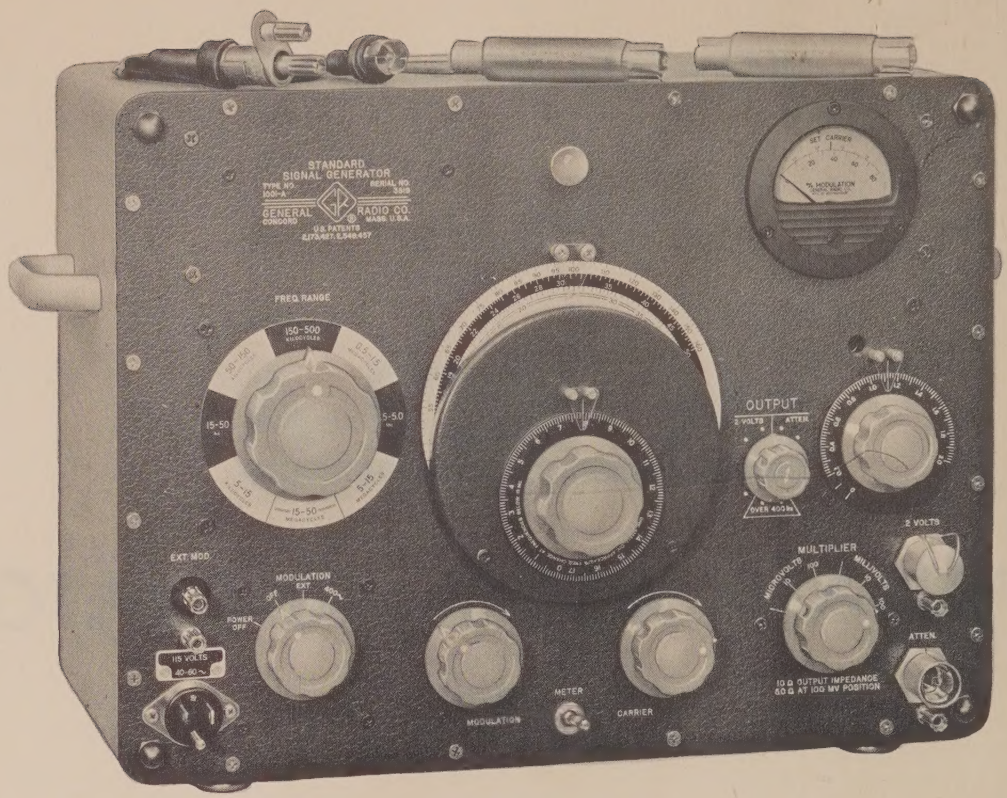
TYPE 1001-A

STANDARD-SIGNAL GENERATOR

Form 1001-0100-L
January, 1962

GENERAL RADIO COMPANY
WEST CONCORD, MASSACHUSETTS, USA



SPECIFICATIONS

Carrier Frequency

Range: 5 kc to 50 Mc covered in eight direct-reading ranges: 5 to 15 kc, 15 to 50 kc, 50 to 150 kc, 150 to 500 kc, 0.5 to 1.5 Mc, 1.5 to 5 Mc, 5 to 15 Mc, and 15 to 50 Mc.

Scale: Logarithmic up to 15 Mc, departing slightly from the logarithmic scale at higher frequencies.

Vernier Dial: Frequency increment is 0.1% per dial division at frequencies up to 15 Mc.

Accuracy: ±1%.

Stability: Warm-up drift is of the order of 0.25%. Half the maximum drift is reached in approximately 1½ hours.

Sweeping: Maximum sweep range with the TYPE 1750-A Sweep Drive is 14%.

Output

Voltage Range: Open-circuit output voltage at the attenuator jack is continuously adjustable from 0.1 microvolt to 200 millivolts. With output cable terminated at both ends, output voltage is continuously adjustable from 0.05 microvolt to 100 millivolts. Open-circuit output voltage at the 2 VOLTS panel jack is measured directly by the output meter and is 2 volts if the meter is set to the reference mark. This voltage is available up to at least 15 Mc.

Voltage Accuracy: At frequencies below 10 Mc, when the output dial is set near full scale or one-tenth full scale, the output voltage is correctly indicated to ± (6% + 0.1 μv). With the output dial set in the mid-scale region, the error may be greater by 4%. At frequencies above 10 Mc, when the output dial is set near full scale, the output voltage is correctly indicated to an accuracy of ± (10% + 0.3 μv) and the error may be as much as 10% larger or smaller at other output dial settings.

The accuracy of the open-circuit output voltages at the 2 VOLTS panel jack is ±3% up to 15 Mc.

Impedance: Output impedance at the attenuator jack is 10 ohms (50 ohms when the series unit is used) except for the highest output position of the attenuator, where it is 50 ohms.

Output impedance at the end of the terminated cable is 25 ohms. Output impedance at the 2 VOLTS panel jack is 300 ohms.

An output impedance of one ohm (with output voltage reduced 100:1) can be obtained with the TYPE 1000-P3 Voltage Divider.

Use of the TYPE 1000-P4 Dummy Antenna provides a standard (IRE) test impedance. A known induction field is obtainable with the TYPE 1000-P10 Test Loop (for testing loop receivers).

Amplitude Modulation: Adjustable from zero to 80%. Modulation percentage is indicated on the panel meter and is accurate within ±10% of the indicated value, with a possible additional error of 2% modulation.

The internal modulation frequency is 400 cps ±5%.

The external modulation characteristic is flat within ±1 decibel from 20 cps to 15 kc. To provide 80% modulation, the external audio oscillator must supply 12 volts into a 4000-ohm load (36 milliwatts).

Incidental Frequency Modulation: At 80% amplitude modulation, the incidental frequency modulation varies from 30 to 300 parts per million over each carrier-frequency range except for the highest range (15 to 50 Mc) where it may be three times as great. At lower modulation percentages, frequency modulation is approximately proportional to modulation percentage.

For applications above 20 Mc, where incidental frequency modulation must be very low, the use of the TYPE 1000-P6 Crystal Diode Modulator is recommended.

Distortion and Noise Level

Envelope Distortion: Less than 8% at 80% amplitude modulation.

Carrier Noise Level: Corresponds to about 0.1% modulation.

Carrier Distortion: Of the order of 7% on all except the lowest range, where it may increase to approximately 15%.

Leakage: Stray fields at 1 Mc are less than one microvolt per meter two feet from the generator.

Tube Complement:

1 - 6C4	1 - 5Y3-GT
1 - 6L6/1614	2 - 0C3
1 - 6AL5	1 - 6SN7-GT

Terminals: TYPE 874 Coaxial Terminals are provided for the attenuator output and for the constant 2-volt output.

Power Input: 105 to 125 (or 210 to 250) volts, 40 to 60 cps. Power input is approximately 65 watts. A three-wire cord is supplied.

This instrument will also operate satisfactorily on power supply frequencies up to 400 cps, provided that the supply voltage is at least 115 volts.

Accessories Supplied: TYPE 874-R22 3-foot Coaxial Cable, TYPE 1000-P1 50-Ohm Termination Unit, TYPE 1000-P2 40-Ohm Series Unit, TYPE 874-Q2 Adaptor, TYPE TO-44 Adjustment Tool (stored in cabinet), TYPE 274-MB Plug, TYPE 874-C58 Cable Connector, TYPE 874-PB58 Panel Connector, spare fuses, and a TYPE CAP-22 Power Cord.

Other Accessories Available: Not supplied but available on order are the TYPE 1000-P3 Voltage Divider, the TYPE 1000-P4 Standard Dummy Antenna, the TYPE 1000-P10 Test Loop, the TYPE 1000-P6 Crystal Diode Modulator, and the TYPE 1750-A Sweep Drive.

Mounting: The instrument is assembled on an aluminum panel, finished in gray crackle lacquer. The aluminum cabinet has a wrinkle finish and has carrying handles. A recessed compartment is built into the top of the cabinet for storing accessories.

Dimensions: Width 20¼, height 13¾, depth 11 inches (515 by 350 by 280 mm) over-all.

Net Weight: 54 pounds (25 kg).

U. S. Patent No. 2,548,457.

TYPE 1001-A
STANDARD-SIGNAL GENERATOR

INTRODUCTION

The Type 1001-A Standard-Signal Generator covers the carrier-frequency range from 5 kc to 50 Mc. It may be amplitude-modulated up to 80% over the audio range from 20 c to 15 kc. The carrier output voltage at the attenuator jack is accurately adjustable to any value from 0.1 microvolt to 200 millivolts; output voltages up to two volts are available at a second jack.

Its major application is in the testing of radio receivers. It can also be used as an r-f voltage standard in field-intensity measurements. Its wide carrier-frequency range makes it suitable for use as a power source in bridge measurements and for measurements on supersonic equipment.

SECTION 1.0 OPERATION

1.1 POWER SUPPLY

The instrument is supplied complete with tubes and is ready for operation.

The line voltage and frequency are indicated on the nameplate above the power-input receptacle. The power-line-frequency range is 40 to 60 cycles. The voltage range is either 105 to 125 or 210 to 250 volts. If it is desired to change from a 105 - 125 volt condition to a 210 - 250 volt condition, or vice versa, change the power-transformer connections as shown in Figure 1, reverse the nameplate to indicate the appropriate line voltage and replace the fuses as specified in the parts list. The fuses are mounted inside the cabinet.

1.2 FREQUENCY CONTROLS

The two frequency controls are the FREQuency RANGE selector switch and the frequency dial. There are eight frequency ranges to cover the spectrum from 4.8 kc to 50 Mc. For rapid identification of the dial scale which corresponds to the selected frequency range, the dial scales and the selector switch segments are alternately etched with light figures on a black background and black figures on a light background except that the 15 - 50 Mc range is identified by a band of two parallel black lines.

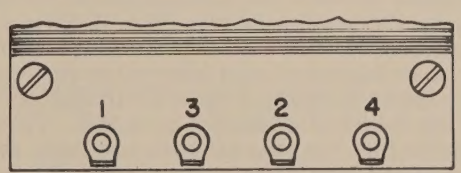
For frequencies up to 15 Mc, the percentage frequency change is proportional to angular rotation. The vernier dial has been calibrated to indicate directly small percentage increments in frequency. Each division of this small dial corresponds to a 0.1% change in frequency except at the ends of the main frequency dial.

1.3 METER ZERO

With the power off, the meter should indicate zero. If it does not, it can be adjusted to zero by means of the screw-driver adjustment on the meter.

With the power ON, the CARRIER control in a full counter-clockwise position and the METER switch at CARRIER, the meter should also indicate zero. If it does not after a minute's warm-up period, and if the "mechanical zero" referred to in the preceding paragraph has been correctly set, the "electrical zero" may be set by means of the screw-driver adjustment available through the small panel hole near the OUTPUT dial (below the panel meter).

With the METER switch at MODULATION and the MODULATION control in a full counter-clockwise position, the meter will indicate zero if the "mechanical zero" referred to above has been correctly set.



CONNECT #1 TO #3 AND #2 TO #4
FOR 105 TO 125 VOLT OPERATION

CONNECT #2 TO #3 FOR 210 - 250
VOLT OPERATION

Figure 1. Power Transformer Connections.

1.4 OUTPUT SWITCH

Output voltage may be obtained either at the 2 VOLTS jack or at the ATTENuator jack. The desired jack is selected by the OUTPUT switch. To prevent leakage, the 2 VOLTS jack should be covered with its shielding cap when the output at the ATTENuator jack is used.

The OUTPUT switch is also used to control the cut-off frequency of a high-pass filter. When the lower index of the OUTPUT switch is at either of the two "OVER 400 KC" positions, modulation-frequency voltage in the output and at the carrier meter is reduced. At carrier frequencies less than 300 or 400 Kc, the OUTPUT switch must be set to one of the two positions beyond the sector marked "OVER 400 KC" and modulation-frequency voltage in the output can be quite high. See paragraphs 1.62 and 2.4.

1.5 OUTPUT ADJUSTMENT WITH NO MODULATION

To obtain output voltage at the ATTENuator jack a fixed carrier level must first be established at the input to the attenuator system by throwing the METER toggle switch to CARRIER and adjusting the CARRIER control until the meter pointer is deflected to the mid-scale point labelled "SET CARRIER". The open-circuit voltage at the ATTENuator jack is then continuously adjustable from 0.1 microvolt to 200 millivolts as shown by the reading of the OUTPUT dial (0 - 2.0) multiplied by the setting of the MULTIPLIER switch.

If the 2 VOLTS jack has been selected by setting the OUTPUT switch to either of the 2 VOLTS positions, the open-circuit voltage appearing at this jack is two volts when the meter is at SET CARRIER. This voltage may be varied by re-adjusting the CARRIER control to obtain the multiplying factors indicated (small numerals) either side of SET CARRIER, but this readjustment may cause a slight change in frequency and an increase in distortion as the output is increased.

1.6 OUTPUT ADJUSTMENT WITH MODULATION

1.61 Modulation Setting: As determined by the setting of the MODULATION switch, the modulating circuits may be connected for 400-cycle modulation from the internal source, for EXTernal modulation (20 to 15,000 cycles) or for no modulation. With the METER switch at MODULATION, the modulation level is indicated on the meter and can be adjusted by means of the MODULATION control to obtain any degree of modulation up to 80%. To provide 80% modulation, the external audio oscillator must be capable of supplying 12 volts into a 4000-ohm load (36 milliwatts).

1.62 Carrier Setting: With the high percentage modulation, the carrier level is reduced a small amount and must be reset by readjusting the CARRIER control if the modulating frequency is 400 cycles or less. At high modulating frequencies, the audio-frequency component in the output voltage will affect the carrier meter reading (particularly when the OUTPUT switch is not at the "OVER 400 KC" sector). To avoid this error, first set the carrier level while using the internal 400 cps at the desired modulation level. Then switch to the external modulation and set the modulation to the desired level, but do not reset the carrier control. The carrier level will be correct even though the carrier meter will not so indicate.

1.7 OUTPUT IMPEDANCE

The output impedance at the ATTENuator jack is 10 ohms for all except the 100 MV MULTIPLIER setting, where the output impedance is 50 ohms.

CAUTION: Care must be taken to prevent the introduction of currents from the circuit under test into the attenuator, since excessive currents (greater than 50 milliamperes) may burn out the attenuator resistance cards.

The circuit impedance at the 2 VOLTS jack is approximately 300 ohms. With the OUTPUT switch at 2 VOLTS, the carrier meter is connected directly across the 2 VOLTS output jack and the effective output impedance is zero.

1.8 OUTPUT CONNECTIONS

When shielded connections are not required at low frequencies, open wires may be connected to the binding posts of the Type 874-Q2 Adaptor (supplied with the instrument) which may be plugged into either the ATTENuator or the 2 VOLTS jack. Similarly, a Type 274-MB Plug may be plugged into either output jack and its associated ground terminal.

At higher frequencies a shielded output cable should be used. The Type 874-R22 3-foot Coaxial 50-Ohm Patch Cord is supplied for this purpose and may be plugged directly into either output jack. The Type 874-Q2 Adaptor may then be plugged into the output end of the patch cord to facilitate connections to the instrument under test; or better still, the Type 874-PB58 Panel Connector or the Type 874-C58 Cable Connector may be installed in the system under test to maintain coaxial connections throughout.

At frequencies above the broadcast range, proper cable termination becomes important. The 50-ohm patch cord is properly terminated at the generator end for the 100-millivolt position of the MULTIPLIER. At other MULTIPLIER positions, the patch cord is properly terminated if the Type 1000-P2 40-ohm Series Unit (supplied with the instrument) is plugged in between the ATTENuator jack and the patch cord. The open-circuit output voltage at the output end of the patch cord is still as indicated by the panel controls but the output impedance is now 50 ohms.

Throughout the range, but in particular at the highest frequencies (10 - 50 Mc), the patch cord may advantageously be terminated at its output end by plugging in the Type 1000-P1 50-ohm Termination Unit. This provides a net output impedance which is lower in value (25 ohms) and more constant with frequency. The output voltage, however, is one-half the voltage indicated by the panel controls.

The Type 874-R22 Patch Cord can be used at the 2 VOLTS jack for frequencies up to 2Mc but should not be terminated.

1.9 SWEEP DRIVE. The Type 1001-A Standard Signal Generator can be swept over a frequency range up to a maximum of 14 percent by means of the Type 1750-A Sweep Drive, which attaches to the slow-motion dial. This Sweep Drive will sweep up to 300 degrees at speeds up to five sweeps per second. An oscilloscope-deflection-voltage circuit provides a horizontal deflection voltage proportional to shaft angle. A blanking circuit eliminates the return trace and produces a base line.

SECTION 2.0 CIRCUIT

2.1 DIAGRAMS

A block diagram is given in Figure 2 and the complete wiring diagram is shown in Figure 3.

2.2 SHIELDING

To reduce leakage and stray fields to a negligible level, the carrier-frequency circuits are contained in a completely closed radio-frequency compartment within the main cabinet. All leads to the radio-frequency compartment are carefully filtered. The two metal shafts that extend from the radio-frequency compartment to the outside of the instrument are well shielded. The cover to the radio-frequency compartment is of double construction with spring contacts bearing on both the inside and outside walls of the compartment.

2.3 CARRIER OSCILLATOR

As shown in the wiring diagram of Figure 3, the Hartley circuit is used in the carrier oscillator. The carrier-frequency range is determined by the setting of a turret which carries the eight range coils and some associated components.

To obtain a compact turret assembly, the coils are mounted alternately on either side of a disc. Each range covers a frequency span of 3.33 to 1 (4.8 to 16 and 15 to 50). The overall range is 4.8 kc to 50 Mc. Since the 100 $\mu\mu$f grid-capacitor (C-4) is too small for the three low-frequency ranges (5 kc - 150 kc), additional capacitance (C-5, C-302) is automatically switched in. The resistor R-2 equalizes the load on the power supply.

The capacitance change of the main tuning capacitor (C-2) is about 750 $\mu\mu$f. The plates are shaped to yield a logarithmic frequency-calibration. To increase mechanical stability, the rotor plates are supported at an unusually large inside diameter. The 15 - 50 Mc range does not utilize the entire capacitance span of the main tuning-capacitor. The calibration for this range does not follow a logarithmic law and the percentage-frequency-change calibration of the vernier dial does not apply.

The oscillator tube is the Type 6C4 Miniature Triode. The amplitude of oscillation, and hence the final output level, are controlled by adjusting the regulated d-c plate-supply of the carrier oscillator by means of R-50, the tapered, 30 kilohm, CARRIER control. The 20 kilohm shunt resistor (R-51) at the CARRIER control equalizes the load on the power supply.

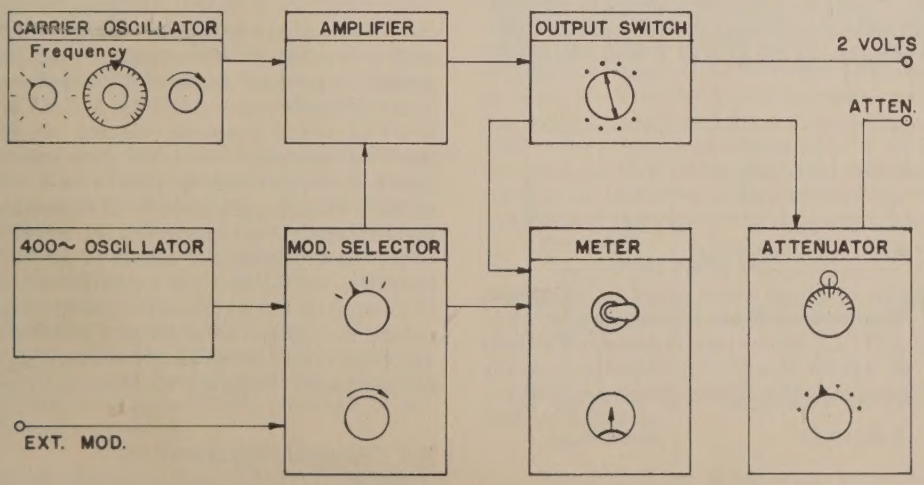


Figure 2. Functional Block Diagram.

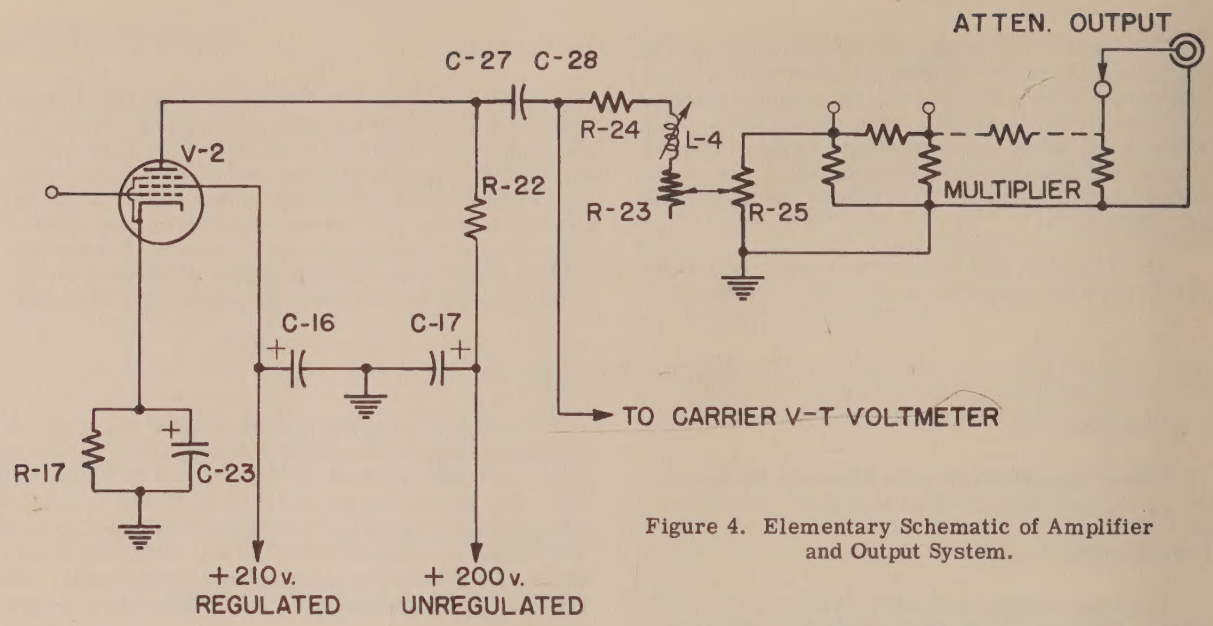


Figure 4. Elementary Schematic of Amplifier and Output System.

The carrier-frequency oscillator is coupled to the amplifier by means of an R-C network to provide the required driving voltage over the entire frequency range. Coupling at high frequencies is adjusted by the small trimmer capacitor C-21.

2.4 CARRIER AMPLIFIER

As shown schematically in Figure 4 and in more detail in the wiring diagram of Figure 3, the 6L6-type beam-power-amplifier tube (V-2) is self-biased and operates as a class A amplifier. The bias due to the voltage drop in R-17 is about -14 volts. The carrier voltage and the modulating voltage are coupled into the grid circuit of the amplifier tube. About 9 volts of audio-frequency voltage are required at the grid of V-2 to obtain 80% modulation. This corresponds to about 12 volts at the EXTernal MODulation terminals. The carrier-frequency voltage required at the grid of V-2 to obtain full output is about 1.6 volts over most of the mid-carrier-frequency range. The plate circuit therefore contains both carrier- and modulation-frequency voltages. To discriminate against modulation-frequency voltages in the signal-generator output and at the carrier voltmeter, coupling capacitor C-27 (500 $\mu\mu$f) is inserted in the plate circuit. Even so, the unwanted voltage can be half of the carrier-frequency voltage for 80% modulation at the maximum modulating frequency (15 kc). As the modulation level and frequency are reduced, the unwanted voltage is reduced rapidly; at 50% modulation and 400 cycles, it is down to one per cent of the carrier voltage. To pass low carrier frequencies which extend down to 5 kc, C-28, a capacitor of 0.01 μf, is added to C-27, and modulation-frequency voltage in the output circuit is increased by a factor of about twenty.

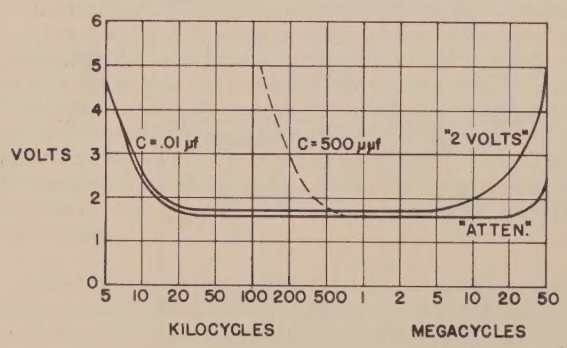


Figure 5. Carrier-Frequency Driving Voltage

The carrier-frequency voltage required at the grid of V-2 depends on the amplifier load and therefore is greater at the extreme ends of the frequency range, particularly at the high end, if the 2 VOLTS position of the OUTPUT switch has been selected. In the ATTENuator position, the load is about 330 ohms and consists of R-23 and R-24 in shunt with the carrier-voltmeter diode V-3a. In the 2 VOLTS positions, R-20 is switched in to obtain higher output; this increases the resistive component of the load to about 410 ohms. Since the coaxial cable leading to the 2 VOLTS jack is also switched in, the load is shunted by the comparatively large capacitance of the cable. For this reason, beyond 10 Mc the driving voltage required at the grid of the amplifier tube (V-2) increases with frequency as shown in Figure 5.

2.5 CARRIER VOLTMETER

A fixed-carrier level is established at the input

to the attenuator system by setting the CARRIER control (R-50) of the carrier oscillator to obtain a SET CARRIER reading on the panel meter. The carrier-voltmeter diode is connected from the high side of R-24 to ground (Figure 3) and yields a SET CARRIER reading at 1.6 volts. When the resistor R-20 is in circuit (OUTPUT switch at 2 VOLTS) the voltage from the high side of R-20 to ground is 2 volts. The carrier voltmeter is essentially a diode (V-3a) in series with the meter and a calibrating resistor; all components have been selected to give accurate calibration over the entire carrier-frequency range of the instrument. The "dummy" diode, V-3b, balances out the contact potential variations of the active diode. As a result, the zero adjustment and calibration are unaffected by normal line voltage variations. The two sections of the Type 6AL5 Miniature Twin-Diode V-3 serve as the "active" diode V-3a and the dummy diode V-3b of the carrier voltmeter. The electrical zero is adjusted by means of the voltage divider R-12 (a screwdriver adjustment that is available at the panel under the meter) and the sensitivity is adjusted by the rheostat, R-52, which is located inside the instrument.

2.6 ATTENUATOR SYSTEM

The attenuator system between the carrier voltmeter and the ATTENuator output jack consists of a continuously adjustable L-type network controlled by the OUTPUT dial and a six-position decade ladder network attenuator which serves as a MULTIPLIER.

The L-type network consists of an inductor (L4), a resistor (R-24), a linear calibrated voltage divider (R-25) and a taper-shaped rheostat (R-23), which maintains the input resistance of the network at 400 ohms as seen from the voltmeter.

Both the rheostat and the voltage divider are Ayrton-Perry wound to reduce the inductance to a minimum. In addition, the voltage divider is mounted on an aluminum block so that it does not act as a one-turn pickup loop when set for zero output.

The L-type network is mounted in the radio-frequency compartment. It is connected to the attenuator (which is mounted on the front panel) through a 274-type plug-and-jack mechanism to permit easy removal of the radio-frequency section from its compartment.

The individual resistors (R-30 through R-39) of the MULTIPLIER attenuator are wound in pairs on small mica cards. Some resistors are wound Ayrton-Perry fashion, and each pair of series and shunt resistors is carefully designed to proportion properly the residual inductances for flat frequency characteristic. The resistance cards are mounted in the segments of a cast housing; the switch contacts are built integrally in the casting for complete shielding between ladder network sections; the switch arm is further shielded from the input to the network by a metal block mounted in the cover of the attenuator housing.

The output impedance as seen at the ATTENuator jack is 10 ohms on all but the 100 MV position of the MULTIPLIER where it is 50 ohms if the calibrated OUTPUT dial of the slide wire (R-25) is set for zero output. At other settings of the OUTPUT dial, the output impedance of the 100 MV position is somewhat less than 50 ohms and reaches a minimum of 43.75 ohms at full-scale setting. This change in output impedance has no effect on the open-circuit output voltage but when using an external termination, it is important to recognize that the impedance varies. Nominally, a 50-ohm termination will halve the output voltage. Actually, when using a 50-ohm termination for the 100 MV position of the MULTIPLIER only, the output voltage may be a maximum of 6-1/2% high unless the following procedure is followed: adjust for SET CARRIER with the MULTIPLIER at any but the 100 MV setting; reset to the 100 MV position; it will be noted that the meter reading will be reduced at the high settings of the OUTPUT dial; if the CARRIER control is not readjusted, the output voltage will be correct.

2.7 MODULATION SYSTEM

The modulation system is shown in Figure 3. The modulating voltage may be obtained from the internal 400-cycle oscillator or from an external generator. The amount of modulation is controlled at the panel by the MODULATION voltage-divider (R-56) and is measured by a crystal-type voltmeter. The modulating voltage is then coupled to the grid of the modulating amplifier through a low-pass filter (see Figure 3).

The internal 400-cycle oscillator is of the R-C type where regeneration from plate to grid through a parallel-T network attenuates all but the desired frequency. The oscillator output is coupled to the grid of a cathode-follower stage and thence to the MODULATION selector switch (S-6). The two sections of a type 6SN7-GT twin-triode tube (V-7) serve as audio-oscillator and as amplifier.

The EXTernal MODulation terminals are connected to the MODULATION selector switch through a low-pass filter which prevents carrier-frequency voltages from appearing at the terminals. With the MODULATION switch at EXTernal modulation (the worst condition) and the MODULATION control on full, the amount of carrier-frequency voltage at the EXTernal MODulation terminals is about 10 μv at 150 kc and decreases very rapidly with frequency to less than 0.1 μv at frequencies above 250 kc. This rapid attenuation with frequency is due not only to the low-pass filter at the EXTernal MODulation terminals but also to the R-C-L filters between the MODULATION control and the grid of the amplifier tube V-2.

The output from the MODULATION control is measured by a full wave rectifier system using two 1N34-AS germanium crystals, D-1 and D-2, and is indicated on the panel meter (M-1). The rheostat R-53 across the meter provides a means for adjusting the calibration, which extends from zero to 80% amplitude modulation.

The R-C filters at the meter terminals and a shield around the meter prevent carrier-frequency leakage.

The audio voltage appearing at the grid of the 6L6-type modulator tube (V-2) inside the r-f compartment must be exactly proportional to the audio voltage measured by the crystal-type modulation voltmeter which is mounted outside the r-f compartment. The two points are coupled through an R-C and an L-C filtering network which has a flat frequency characteristic over the audio range up to 15 kc and discriminates sharply against higher frequencies.

2.8 ACCESSORIES

All accessories use the universal Type 874 Coaxial Connectors which eliminate the mechanical matching difficulties inherent in conventional plug-and-jack designs.

The Type 874-R22 Patch Cord is a double-shielded 3-foot 50-ohm coaxial cable of approximately 32 $\mu\mu$f per foot capacitance.

The Type 1000-P1 Termination Unit contains a 50-ohm resistor connected in shunt from the central conductor to the coaxial outer conductor. This unit is intended for proper termination of the Type 874-R22 Patch Cord at the output end.

The Type 1000-P2 Series Unit contains a 40-ohm resistor connected in series with the central conductor. This unit is used to increase the 10-ohm output impedance of the ATTENuator jack at all but the 100 MV position to 50-ohm output impedance for proper matching to the Type 874-R22 Patch Cord at the signal generator end.

The Type 874-Q2 Adaptor is used to connect leads to the two output jacks of the signal generator or to the output end of the Type 874-R22 Patch Cord.

SECTION 3.0 METHODS FOR RECEIVER TESTING

3.1 METHODS

Several methods for testing broadcast receivers have been recommended by the Institute of Radio Engineers (One East 79th Street, New York 21, New York) in the 1948 version of the Standards on Radio Receivers, Methods of Testing Amplitude-Modulation Broadcast Receivers and in the Standards published in the September, 1955 IRE PROCEEDINGS: "Method of Testing Receivers Employing Ferrite Core Loop Antennas." The test procedures include the use of a standard dummy antenna for testing receivers designed for a conventional overhead-type of antenna and a test loop for testing receivers designed for use with a loop antenna.

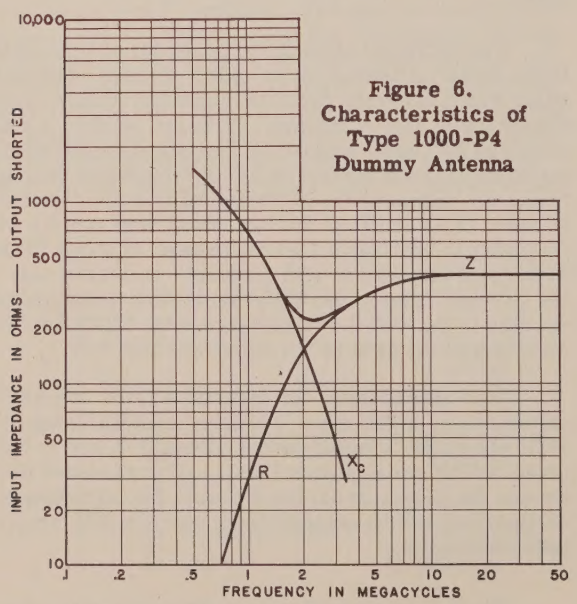


Figure 6. Characteristics of Type 1000-P4 Dummy Antenna

3.2 STANDARD DUMMY ANTENNA

When the receiver tests require the use of a standard dummy antenna, the Type 1000-P4 Standard Dummy Antenna (not supplied as standard equipment with the instrument) should be connected directly to the receiver antenna terminals (by means of the Type 874-Q2 Adaptor, if need be). The Type 1000-P4 Standard Dummy Antenna is built into a small cylindrical shield and gives the impedance-frequency characteristic shown in Figure 6 with the component values selected as shown in Figure 7 when working out of a 25-ohm source impedance. The Type 1001-A Standard-Signal Generator provides the correct source impedance (25 ohms) when the patch cord is terminated with the Type 1000-P1 50-Ohm Termination Unit. For all but the 100 MILLIVOLT positions, the Type 1000-P2 40-Ohm Series Unit must be connected between the generator and the patch cord. Since the cable is terminated, the output voltage is one-half the voltage indicated by the panel settings.

At the highest frequencies (15 - 50 Mc), if coaxial connections cannot be maintained up to the receiver input terminals, errors in sensitivity measurements can result due to the reactance of the connecting leads. A method for introducing a measured amount of power into the receiver input terminals, in spite of appreciable lead reactance, is described in RCA APPLICATION NOTE number AN 132 of May 17, 1948, entitled, "Receiver Sensitivity and Gain Measurements at High Frequencies". In this method, when the receiver tuning capacitor and

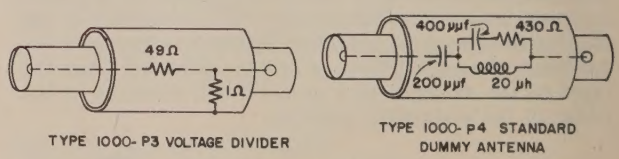


Figure 7.

an externally added series capacitor are both tuned for maximum receiver output, the receiver presents an effective input resistance which matches the dummy antenna resistance, and the input power may then be calculated.

3.3 LOOP ANTENNA - LOW IMPEDANCE METHOD

When the receiver under test is equipped with a loop antenna, it may be tested either with a transmitting test loop connected to the standard-signal generator or by introducing the test signal into the receiver loop through a very low impedance generator.

The Type 1000-P3 Voltage Divider (not supplied as standard equipment with the Type 1001-A Generator) was designed to facilitate the injection of a test signal in series with the receiver loop. The voltage divider is shown schematically in Figure 7. Its 50-ohm impedance at one end of the unit effectively terminates the Type 874-R22 50-Ohm Coaxial Patch Cord and its one-ohm impedance at the other end of the unit is sufficiently low for insertion in series with the receiver's loop antenna without disturbing its normal operation. The voltage appearing at the one-ohm, or loop end of the voltage divider is one hundredth of the voltage indicated by the panel control settings (remember to use the Type 1000-P2 40-Ohm Series Unit at all but the 100 MV MULTIPLIER settings). CAUTION: This method is not recommended for use with the ac-dc type of receiver where one side of the power line is connected directly to the receiver chassis. There is considerable shock hazard if the signal generator is operated ungrounded; there is also the danger that the attenuator cards may be burned out.

3.4 LOOP ANTENNA - TEST LOOP METHOD

The Type 1000-P10 Test Loop (not supplied as standard equipment with the Type 1001-A Generator) provides a convenient means for measuring loop-antenna receivers in accordance with the preferred method outlined in the I.R.E. Standards mentioned above.*

The Type 1000-P10 Test Loop is an electrostatically shielded, three-turn coil of ten inches diameter. Figure 8 shows a schematic of the loop and its coupling

*See also "Measurement of Loop-Antenna Receivers" W. O. Swinyard, Proc. I.R.E., p. 382, July 1941 and "Calibration of Loop Antenna at VLF", A. G. Jean, H. E. Taggart, and J. R. Wait, Journal of Research of the National Bureau of Standards, C. Engineering and Instrumentation, Vol. 65, No. 3, July-September, 1961.

Figure 8.

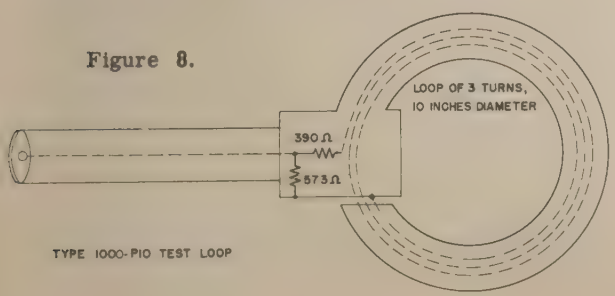
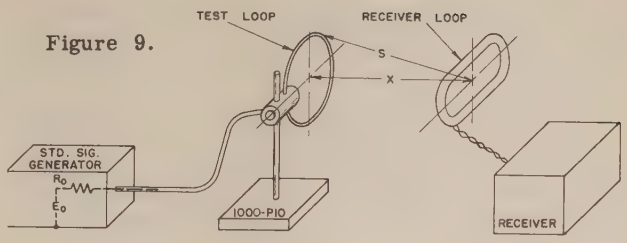


Figure 9.



circuit. The three-turn loop is connected to a four-foot coaxial cable by a 390-ohm resistor to assure constant loop current for a given input voltage up to 3 Mc. The 50-ohm cable is effectively terminated by the 50-ohm shunt combination of a 57.3-ohm shunt resistor and the 390-ohm series resistor. The input to the cable utilizes a Type 874-C Cable Connector.

Figure 9 shows the proper arrangement of apparatus for testing a loop-antenna radio-receiver with a standard-signal generator and the Type 1000-P10 Test Loop.

Note that the loops are arranged coaxially. The separation between the loops should be at least twice the greatest dimension of the larger loop.

The equivalent electric field intensity in microvolts per meter at the center of the receiving loop antenna is:

$$E = \frac{71{,}250}{(50 + R_o)S^3} E_o$$

Where E_o is the open-circuit output voltage of the standard-signal generator in microvolts, R_o (ohms) is the output impedance of the standard-signal generator, and S (inches) is the separation between the test loop and the receiving loop, as shown in Figure 9.

It is usually convenient to select the separation between loops so that the field intensity is readily expressed in terms of the signal generator voltage, E_o. For example, when using the Type 1001-A Standard-Signal Generator with its 50-ohm output impedance, the field intensity in microvolts per meter at the receiver loop antenna is one-tenth of the open-circuit output voltage of the generator if the two loops are approximately one-half meter apart. Thus, when the signal generator open-circuit output voltage as indicated on the panel controls is 100 microvolts, the field intensity at the receiver loop is ten microvolts per meter.

Table I lists the loop spacing required under various generator impedance (R_o) conditions to obtain a convenient factor for determining the field intensity (E) at the receiving loop antenna in terms of the signal generator open-circuit output voltage, E_o.

The separation "S" between loops is the distance between the outer periphery of the test loop and the center of the receiving loop. The separation "X" between loop centers is somewhat less, as shown in Table I.

TABLE I

R_O	E_O/E	S (inches)	X (inches)
0 Ω	5	19.3	18.7
	10	24.2	23.7
	20	30.6	30.2
	50	40.9	40.5
	100	52.2	52.0
10 Ω	10	22.8	22.2
	20	28.8	28.4
	50	39.0	38.6
	100	49.2	49.0
37.5 Ω	10	20.1	19.4
	20	25.4	24.8
	50	34.4	34.0
	100	43.3	43.0
	200	54.6	54.3
50 Ω	10	19.3	18.7
	20	24.2	23.7
	50	32.9	32.5
	100	40.9	40.5
	200	52.2	52.0
75 Ω	20	22.5	22.0
	50	30.6	30.2
	100	38.5	38.1
	200	48.5	48.2

3.5 LOOP ANTENNA - TRANSMISSION-LINE METHOD

In this method, a transmission line is formed by stretching a single solid wire (#12 to #16 B and S gauge) between two insulators in a shielded room at a constant spacing from the ceiling. The transmission line is terminated at one end and fed from the standard-signal generator at the other end.

The method is described in the Appendix (Section 6.0) of the 1948 version of the IRE Standards referenced in paragraph 3.1 above.

Refer to Figure 10. The standard-signal generator is located outside the shielded room and is connected to the transmission line by means of a shielded cable grounded at the shielded room.

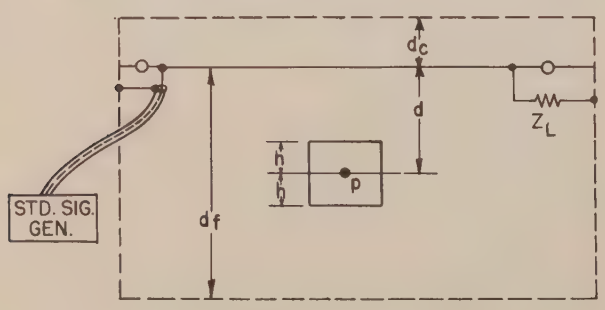


Figure 10.

The terminating resistance Z_L is equal to the line impedance

$$Z_L = Z_O = 138 \log_{10} \frac{4 d_c}{a}$$

where "d_c" is the distance from the wire to the ceiling and "a" is the diameter of the wire. A 1000-ohm rheostat may be satisfactory as a termination. It is adjusted to the correct value when a vacuum-tube voltmeter indicates constant voltage (no standing waves) along the wire. This adjustment should be made at the highest operating frequency.

The field strength E in microvolts per meter at a point P directly below the center of the wire and near the center of the room is

$$E = \frac{60 E_g}{Z_g + Z_O}\left[\frac{1}{d} - \frac{1}{2d_c + d} + \frac{1}{2d_f - d} - \frac{1}{2d_f + 2d_c - d} + \frac{1}{2d_f + 2d_c + d} - \frac{1}{2d_f + 4d_c + d} + \frac{1}{4d_f + 2d_c - d} - \frac{1}{4d_f + 4d_c - d} \cdots\cdots\right]$$

where E_g = signal generator output in microvolts
Z_g = signal generator impedance
d = distance in meters from wire to point P
d_f = distance in meters from wire to floor
d_c = distance in meters from wire to ceiling

If a square loop is used, the average field strength around the loop is approximately

$$E_{ave} = \frac{60 E_g}{Z_g + Z_O}\left[\frac{d}{2h} \log_e \frac{d + h}{d - h}\right]\left[\frac{1}{d} - \frac{1}{2d_c + d} + \frac{1}{2d_f - d} - \frac{1}{2d_f + 2d_c - d}\right]$$

where "2h" is the height of one side of the loop.

3.6 FERRITE-CORE LOOP ANTENNA

The Type 1000-P10 Test Loop (described in paragraph 3.4) is recommended for measuring ferrite-core loop-antenna receivers in accordance with the method outlined in the IRE Standard: "Method of Testing Receivers Employing Ferrite Core Loop Antennas."*

The correct arrangement of the apparatus is shown in Figure 11. The indicated orientation of the apparatus assures a substantially constant field at the ferrite-core loop antenna. Measurements should be carried out in a shielded room.

The equivalent electric field intensity in microvolts per meter at the receiver loop is

$$E = \frac{35{,}625}{(R_O + 50)X^3} E_O$$

*PROCEEDINGS OF THE IRE, Vol 43, No. 9 (Sept., 1955) pp. 1086-1088.

where E_0 is the open-circuit output voltage of the standard-signal generator in microvolts, R_0 (ohms) is the output impedance of the standard-signal generator and X is the distance (in inches) from the center of the Type 1000-P10 Test Loop to the center of the ferrite-rod loop antenna.

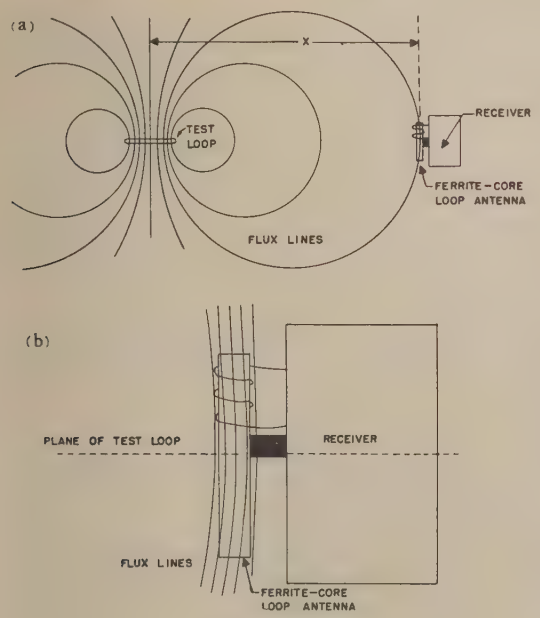


Figure 11.

Table II lists the loop spacing required under various generator-impedance (R_0) conditions to obtain a convenient factor for determining the field intensity (E) at the receiving ferrite-rod loop antenna in terms of the signal-generator open-circuit voltage, E_0, when using the Type 1000-P10 Test Loop.

TABLE II

R_0	E_0/E	X(inches)	R_0	E_0/E	X(inches)
0 Ω	5	15.3	37.5 Ω	50	27.2
	10	19.3	(Cont.)	100	34.3
	20	24.2		200	43.4
	50	33.0	50 Ω	5	12.1
	100	41.5		10	15.3
	200	52.4		20	19.3
10 Ω	5	14.4		50	26.2
	10	18.1		100	33.0
	20	22.8		200	41.5
	50	31.0	75 Ω	5	11.2
	100	39.0		10	14.1
	200	49.0		20	17.8
37.5 Ω	5	12.6		50	24.2
	10	15.9		100	30.5
	20	20.0		200	38.4

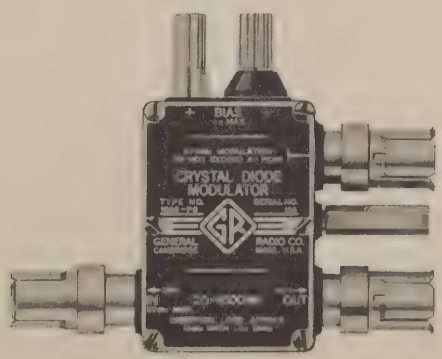
SECTION 4. ACCESSORY AMPLITUDE MODULATOR

4.1 MODULATION METHODS

The Type 1001-A Generator is normally amplitude-modulated in the grid circuit of its amplifier tube (V-2). There is some incidental frequency modulation (see specifications). While the magnitude of incidental frequency modulation is relatively small, it may be excessive for some applications. Amplitude modulation free of incidental fm can be obtained at carrier frequencies above 10 Mc by using a Type 1000-P6 Crystal Diode Modulator as outlined below.

4.2 TELEVISION MODULATOR

In the Type 1000-P6 Crystal Diode Modulator,# the resistance of a 1N21-B type crystal to radio-frequency current is a function of the modulating-frequency voltage across it. As a consequence, the radio frequency output of a Type 1001-A Generator can be amplitude modulated with no incidental fm if the Type 1000-P6 Modulator is connected at the output terminals of the generator. The modulating-frequency characteristic is flat from zero up to several megacycles and it is down only 2 db at 5 megacycles which makes it possible to test at the television intermediate frequency with the Type 1001-A Generator. A convenient source of video modulation voltage is a television receiver tuned to a local station. The Type 1000-P6 Modulator is fitted with Type 874 Coaxial Terminals for the input and output connections and for the modulation circuit. The modulation range is from zero to about 50%; it is not indicated on a meter. The modulator is designed to operate from a 50-ohm source into a 50-ohm load. To avoid distortion, the radio-frequency input to the crystal modulator must be limited to 50 millivolts. The insertion loss is approximately 12 db over the radio-frequency range of 20 - 1000 Mc and it increases to approximately 20 db at 10 Mc.



Type 1000-P6 Crystal Diode Modulator

#W. F. Byers, "A Simple Amplitude Modulator", General Radio Experimenter, March 1950.

SECTION 5.0 WIDE-BAND AMPLIFIER TESTS

5.1 EFFECT OF VARYING CARRIER DISTORTION

When a standard-signal generator is used in wide-band amplifier measurements, the usual test procedure is to set the generator voltage at the desired level as indicated by the attenuator settings and by the carrier meter in the generator; the amplifier output is then measured with an external meter. A gain-frequency curve plotted from data obtained from these measurements may exhibit discontinuities at those frequencies where the range switch position of the Type 1001-A Generator is changed. The discontinuities in indicated gain are due to differences in magnitude and character of the carrier distortion and percentage-wise may exceed appreciably the amount of distortion. The carrier meter in the generator is of the low impedance type with a response somewhere between average and positive peak. The response of the external meter may be any one of several types such as positive or negative peak, average, r.m.s., full-wave, half-wave, low or high impedance with consequent varying accentuation of the discontinuities.

Discontinuities and errors in gain measurements are reduced considerably or completely avoided by using the same meter (or two similar meters) to measure both the input and output voltages of the amplifier under test. The output system of the Type 1001-A Generator is well adapted to such a procedure, as outlined below, if complete shielding of the input to the amplifier is not required.

5.2 TEST PROCEDURE

Set the OUTPUT switch of the Type 1001-A Generator to 2 VOLTS. Connect the amplifier under test to the ATTENuator jack. Connect a high impedance voltmeter to the 2 VOLTS jack. Use this external meter rather than the internal carrier meter to monitor the input to the attenuator system; disregard the readings of the internal carrier meter. Adjust the CARRIER control to obtain 2 volts on the external meter. Set the OUTPUT dial and MULTIPLIER (attenuator) to the desired amplifier input voltage. Measure the amplifier output voltage with the same external meter or with another meter of similar response characteristics. The amplifier gain is the ratio of the amplifier output voltage to the signal generator output voltage as shown by the output dial and attenuator settings.

Amplifier gain-frequency curves plotted from data obtained by the above procedure will be free of discontinuities unless the amplifier under test introduces appreciable phase shifts. Since each amplifier stage normally produces a 180 degree phase shift, the external meter connections may have to be transposed at either the 2 VOLTS jack or at the amplifier output terminals when the amplifier consists of an odd number of stages. With some power-line operated meters, this transposition may introduce serious loading errors which can be avoided by using a battery operated instrument.

SECTION 6.0 SERVICE AND MAINTENANCE NOTES

6.1 GENERAL. The two-year warranty given with every General Radio instrument attests the quality of materials and workmanship in our products. When difficulties do occur, our service engineers will assist in any way possible.

In case of difficulties that cannot be eliminated by the use of these service instructions, please write or phone our Service Department, giving full information of the trouble and of steps taken to remedy it. Be sure to mention the serial and type numbers of the instrument.

Before returning an instrument to General Radio for service, please write to our Service Department or nearest district office (see back cover), requesting a Returned Material Tag. Use of this tag will ensure proper handling and identification. For instruments not covered by the warranty, a purchase order should be forwarded to avoid unnecessary delay.

6.2 SERVICE. If the Signal Generator becomes inoperative, preliminary tests should be made before the instrument is disassembled. Inspect the power source to determine if the instrument is receiving power. Measure voltage at the output end of the line cord and check the cord connection to the instrument power receptacle. Under operating conditions the instrument draws 65 watts on a 115-volt line. Remove the instrument from the cabinet (paragraph 6.3) and inspect line fuses and holders. The fuses are in the rear of the instrument, below the shielded r-f section.

6.3 DISASSEMBLY AND REASSEMBLY.

6.3.1 REMOVAL OF INSTRUMENT FROM CABINET. To remove the instrument from the cabinet, unfasten all bright-nickle-plated machine screws along the edges of the panel (16 screws in all). When the instrument is re-

placed in the cabinet, tighten all these screws equally to minimize r-f leakage. A recommended torque to be applied to these screws is 15 inch-pounds.

6.3.2 REMOVAL OF R-F UNIT. Remove the spring-held shielded cover on the rear of the r-f section by pushing it away from the panel. The r-f unit is so designed that it can be operated outside of the instrument, by the use of a built-in interconnecting cable, which is wound on the front of the r-f unit. Should the r-f unit be removed, frequency calibration and output dial readjustment will be necessary when the r-f unit is returned to the instrument. Before any disassembly is undertaken, set the attenuator MULTIPLIER to 100 millivolts and the output dial to exactly 1.0. Then proceed as follows:

a. With an accurate bridge that can measure to the nearest hundredth of an ohm, measure the d-c resistance between the high side of the ATTENUATOR terminal and the contact arm of R23, the potentiometer mounted on the r-f unit. Record this value, which will be used later for resetting the output dial correctly. The value of d-c resistance will be in the vicinity of 36.50 ohms.

b. Remove the output dial, OUTPUT knob, FREQUENCY RANGE knob, and associated parts.

c. To remove the main frequency dial, first unfasten the two screws holding the dial cover plate and knob assembly. Lift off the cover plate and remove the main dial by loosening the setscrews in the hub.

d. Disconnect the cable leading from the two-volt terminal to the r-f compartment by loosening the feedthrough bushing and the screw terminal connection inside the r-f compartment.

e. Remove the four large screws from the tubular standoffs at the rear of the r-f shelf.

f. Pull out the r-f unit.

g. If the two screws that mount the seven-terminal plug plate on the r-f unit are removed, the plug plate can be connected to the instrument and the r-f unit can be operated outside of the instrument for easier servicing.

6.3.3 REASSEMBLY.

a. Before replacing the r-f unit in the compartment, wind the service cable back onto the supports provided. Remount the seven-terminal plug plate.

b. Fasten the r-f unit in the compartment and note if any shaft binds. If there is bind, loosen and retighten the panel screws that hold bearing plates coaxially about the shafts.

c. Replace the two-volt cable and bushing.

d. Replace FREQuency RANGE and OUTPUT knobs. Make sure that the insulated sleeve, bakelite block, spring washer and 3/4-in. collar are mounted on the frequency range selector shaft. The flat on the shaft indicates the arrow side of the knob.

e. Mount frequency range knob assembly as flush as possible to the panel to minimize r-f leakage.

f. Mount the main frequency dial, insulated sleeve, and spring washer. Slightly tighten one of the set screws on the dial hub. Set the main tuning capacitor to full mesh by butting the rotor plates against a straight-edge held firmly on the stator plates. Slip the frequency dial until the reference line on the dial lines up with the hairline on the indicator. The reference line is located on the dial, six degrees below the lowest frequency mark. Tighten the dial setscrews, making sure that the dial assembly is flush with the panel. Attach the cover plate.

g. Mount the spring washer and the 5/16-in. collar on the output control shaft. With the attenuator MULTIPLIER at the 100-millivolt position, set the output control to the previously recorded value of resistance. Return the output dial to the shaft and set it for a reading of 1.0. Be sure that the dial assembly is tightened as flush as possible to the panel to minimize r-f leakage.

6.4 TROUBLE-SHOOTING.

6.4.1 INSTRUMENT INOPERATIVE.

a. Check that the pilot light and all tube filaments are lighted.

b. Test V1, V2, V3, V4, and V7. The voltage regulator tubes V5 and V6 should emit a steady glow.

c. Measure voltages on transformer T1 (see Table 1).

d. Check that resistors R47, R48, and R49 are not open-circuited.

e. Measure tube voltages (see Table 2).

f. Measure resistances (see Table 3).

6.4.2 GENERATOR DRAWS EXCESSIVE POWER AND BLOWS FUSES.

a. Inspect the power supply for short circuits.

b. Test the Type 5Y3 rectifier tube V4 for internal shorts.

c. Check filter capacitors C34 through C38 for short circuits or low leakage resistances.

d. Check all plate supply wiring for broken insulation and visible short circuits.

e. Check that capacitors C8, C9, C10, C11, C12, and C14 are not shorted.

6.4.3 NO CARRIER READING.

a. Inspect the action of all contacts on the coil turret mechanism. These should operate properly for both directions of turret rotation. Check the oscillator coils with an ohmmeter for continuity.

b. Test V1, V2, and V3.

c. Measure the output of the oscillator from pin 1 of the Type 6C4 tube V1 to ground with a vacuum-tube voltmeter, such as GR Type 1800-B. Output should be approximately 7 volts ac (at 1 megacycle).

d. Check voltages of V1, V2, and V3.

e. Check capacitors C16, C17, and C18 for short-circuits.

f. If there is output and the meter does not read, check V3. If V3 is all right and there is no carrier indication, test the meter. DO NOT CHECK METER CONTINUITY WITH AN OHMMETER. The meter will read full scale on 200 microamperes of direct current.

g. If the carrier meter is defective, a replacement should be ordered from the General Radio Service Department. General Radio Company cannot assume responsibility for any local repairs to the meter, although such repairs may be necessary in an emergency.

6.4.4 CARRIER OUTPUT ERRATIC.

a. Check the action of all finger contacts on the coil turret. Look for foreign matter and dirt on the contact surfaces.

b. Clean out any foreign matter that may be lodged between plates of the main tuning condenser C2.

c. Inspect the operation of the wiping contact on the main tuning condenser C2.

d. Check that voltage regulator tubes V5 and V6 are operating with a steady glow. (Voltage regulator tubes may flicker on abnormally low line voltages.)

6.4.5 NO MODULATION READING ON METER.

a. With a suitable means of detection (radio receiver or cathode-ray oscilloscope) determine the presence of modulation on the carrier. If the carrier is modulated but the meter does not read, measure the front and back resistances of the crystal diodes D1 and D2. The ratio of front to back resistance is approximately 1 to 50 (measured on the X100 Ω scale of a multimeter). Replace any diode that exhibits a low front to back resistance ratio. If there is no reading on both the carrier and modulation positions and output exists, check the meter. DO NOT USE AN OHMMETER IN CHECKING METER CONTINUITY. The meter will read full scale with 200 microamperes of direct current applied. Refer to paragraph 6.4.3g.

b. If the meter does not read and the carrier is not modulated, test the oscillator-amplifier tube V7. Measure resistors R65, R66, R67 and capacitors C43, C44, and C45.

6.4.6 NO MODULATION OF CARRIER (METER READS).

a. If no modulation appears in the output, measure the grid voltage at pin 5 of V2 with a vacuum-tube voltmeter. Voltage should be approximately 11 volts for 80% modulation. Test V2.

b. Measure the voltage across C14. It should be at least 12 volts for 80% modulation.

6.4.7 ERRATIC MODULATION.

a. Replace tube V2. The replacement for this tube must be selected for low distortion.

b. Check capacitors C8, C9, C10, C11, C12, C14, C16, C17, C18, and C23.

6.4.8 MEASUREMENT OF ATTENUATOR RESISTORS. Set the OUTPUT dial to zero and the OUTPUT switch to ATTENuator. Measure the d-c resistance across the ATTENuator output with an accurate bridge. It should be 50 Ω ±1.5% on the 100-millivolt position and 10 Ω ±0.75% on the other multiplier settings.

6.5 FREQUENCY CALIBRATION. Frequency adjustments can be made through holes found under a spring strap in the top of the r-f compartment shield. The adjustments for the various frequency ranges are found as follows:

Frequency	Inductor Core Adjustment (hex-wrench adjustment	Trimmer Adjustment (screw-driver adjustment
5-15kc	hole A	hole B
15-50kc	D	C
50-150kc	A	B
150-500kc	D	C
0.5-1.5Mc	A	B
1.5-5.0Mc	D	C
5-15Mc	A	B
15-50Mc	D	C

The procedure for frequency calibration is as follows:

a. First adjust the low-frequency end of a given range with the appropriate inductor core adjustment. A hex wrench (Tool No. TO-44), provided for this purpose, is clip-mounted inside the cabinet. Turning the core clockwise results in a corresponding decrease in frequency at a given point on the dial. In other words, if the actual frequency falls below its calibrated point on the dial, a clockwise adjustment will bring the frequency and the calibration into agreement.

b. When the low end of the range is satisfactorily adjusted, tune the instrument to the high end of the range and note relative positions of various frequencies with respect to calibrated points on the dial. A screw-driver adjustment of the trimmer condensers will bring the frequency and the calibration into agreement.

c. Spot check various frequencies along the dial to determine over-all accuracy. Repeat calibration procedure if necessary.

6.6 TUBE REPLACEMENT. If the 6C4 oscillator tube (V1) is replaced, the frequency calibration at the high-frequency end of each range may need adjustment. Refer to paragraph 6.5 for procedure.

The filaments of replacement 6AL5 voltmeter tubes (V3) should be aged for at least 24 hours. Upon replacement it may be necessary to recalibrate the voltmeter.

The procedure is as follows:

a. Adjust the meter mechanical zero.

b. Turn on the power, set the METER switch to CARRIER, the frequency to 600 kc, and the OUTPUT switch to 2 volts over 400 kc. Short-circuit resistor R20 and allow the instrument to warm up before making any adjustments. Resistor R20 is mounted on switch S2.

c. Adjust the electrical zero, and connect a carefully calibrated rms-reading vacuum-tube voltmeter to the 2-VOLT OUTPUT jack. Adjust CARRIER control for 1.52 volts at the vacuum-tube voltmeter. Adjust potentiometer R52 (located at the rear of instrument and labeled "CARRIER") to obtain a panel-meter reading at the SET CARRIER line. Recheck the electrical zero.

d. Remove the short-circuit from across resistor R20, reset the CARRIER control to obtain "SET CARRIER" reading on panel meter and check that the vacuum-tube voltmeter reads 1.9 volts ±3%.

6.7 INSTRUMENT MODIFICATIONS. Instruments manufactured prior to March 1952 may have excessive 60-cycle voltage at the output terminals. This may show up as a 60-cycle modulation on the carrier or as an inability to attenuate the output to 0.1 microvolt. If this should occur the following changes can be made:

a. Remove the lead from terminal 12 to terminal 17 of transformer T1. Remove the ground connection at pin 8 of V7, the ground lead of V7, and the ground lead of the carrier potentiometer R50.

b. Ground terminal 17 of transformer T1, pin 8 of V7, and the ground side of R50 at a common terminal on the oscillator shield. It is suggested that they be grounded to a terminal added to the mounting screws of either C8, C10, or C11. These capacitors are found mounted on top of the r-f compartment.

6.8 VOLTAGE MEASUREMENTS.

TABLE 1

Transformer T1 Voltage Measurements

Between Term. No.	Term. No.	A-c Volts
11	13	630
14	16	4.3
17	18	6.3
11	Ground	315
13	Ground	315
14	Ground	700
15	Ground	700
16	Ground	700

TABLE 2
Voltage Chart

Tube, Type	RANGE	Pin. No. 1	2	3	4	5	6	7	8	Tube Function
V1 (6C4)	5-15kc	25	-	6.0vac	0	-	-3.5	0.1		R-F OSC
	15-50kc	15	-	6.0vac	0	-	-2.5	0.1		
	50-150kc	17	-	6.0vac	0	-	-2.7	0.1		
	150-500kc	23	-	6.0vac	0	-	-2.4	0.1		
	0.5-1.5Mc	32	-	6.0vac	0	-	-10.0	0.2		
	1.5-5Mc	34	-	6.0vac	0	-	-5.5	0.2		
	5-15Mc	62	-	6.0vac	0	-	-3.5	0.6		
	15-50Mc	112 (7.5vac)	-	6.0vac	0	-	-1.6	1.4		
V2 (6L6 or 1614)	0.5-1.5Mc	0	6.0vac	143 (2.2vac)	205	0 (0.8vac)	0	0	15.5	MIXER AMPLIF
V3 (6AL5)	0.5-1.5Mc	0.54	-0.06	6.0vac	0	1.6	0.1	0.4		VTVM DIODE
V4 (5Y3)	0.5-1.5Mc	-	330	-	300vac	-	300vac	-	330	RECT
V5 0C3)	0.5-1.5Mc	-	107	-	-	212	-	-	-	REG
V6 (0C3)	0.5-1.5Mc	-	0	-	-	107	-	-	-	REG
V7 (6SN7)	0.5-1.5Mc 400~Mod.On	0	81	2.5	58	260	118	6.0vac	0	AUDIO OSC and AMPLIF
	Mod. Off	0	66	2.7	58	270	120	6.0vac	0	

NOTES

1. Line voltage 115 v, 60 cps
2. Voltages dc unless otherwise specified.
3. Measure with vacuum-tube voltmeter (GR Type 1800 recommended)
4. Range settings as noted.
5. Modulation frequency 400 cps, with 80% modulation.
6. CARRIER pot.- to SET CARRIER line on each range.
7. OUTPUT switch at appropriate ATTENuator setting.
8. Output slide wire set to zero.
9. MULTIPLIER - 100 mv
10. Main tuning dial set to 100 on outer scale.

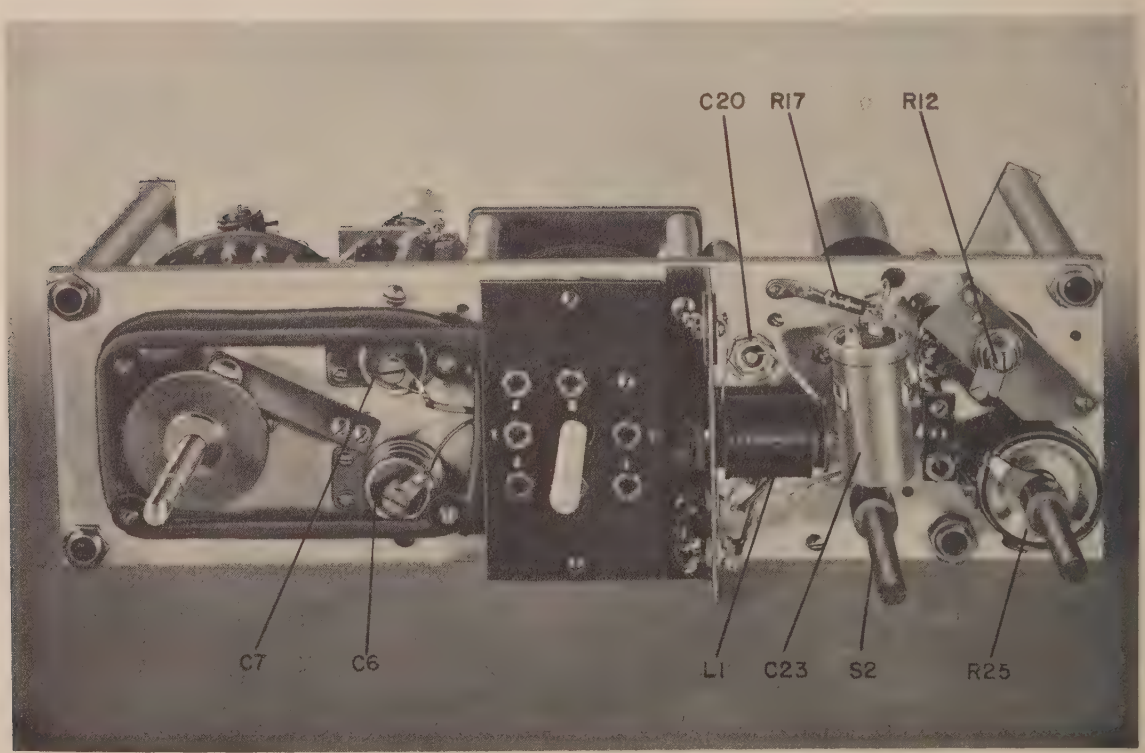
TABLE 3
Resistance Chart

	Pin. No							
Tube	1	2	3	4	5	6	7	8
V1	280*	-	0	0	-	100k	300	
V2	0	0	7.5k	280	65k	10k**	0	360
V3	6k	400	0	0	∞	1k	∞	
V4	-	3k	-	120	-	120	-	3k
V5	-	∞	-	-	0	-	-	
V6	-	0	-	-	∞	-	-	
V7	10M	130k	2.6k	1.5M	4.5k	28k	0	

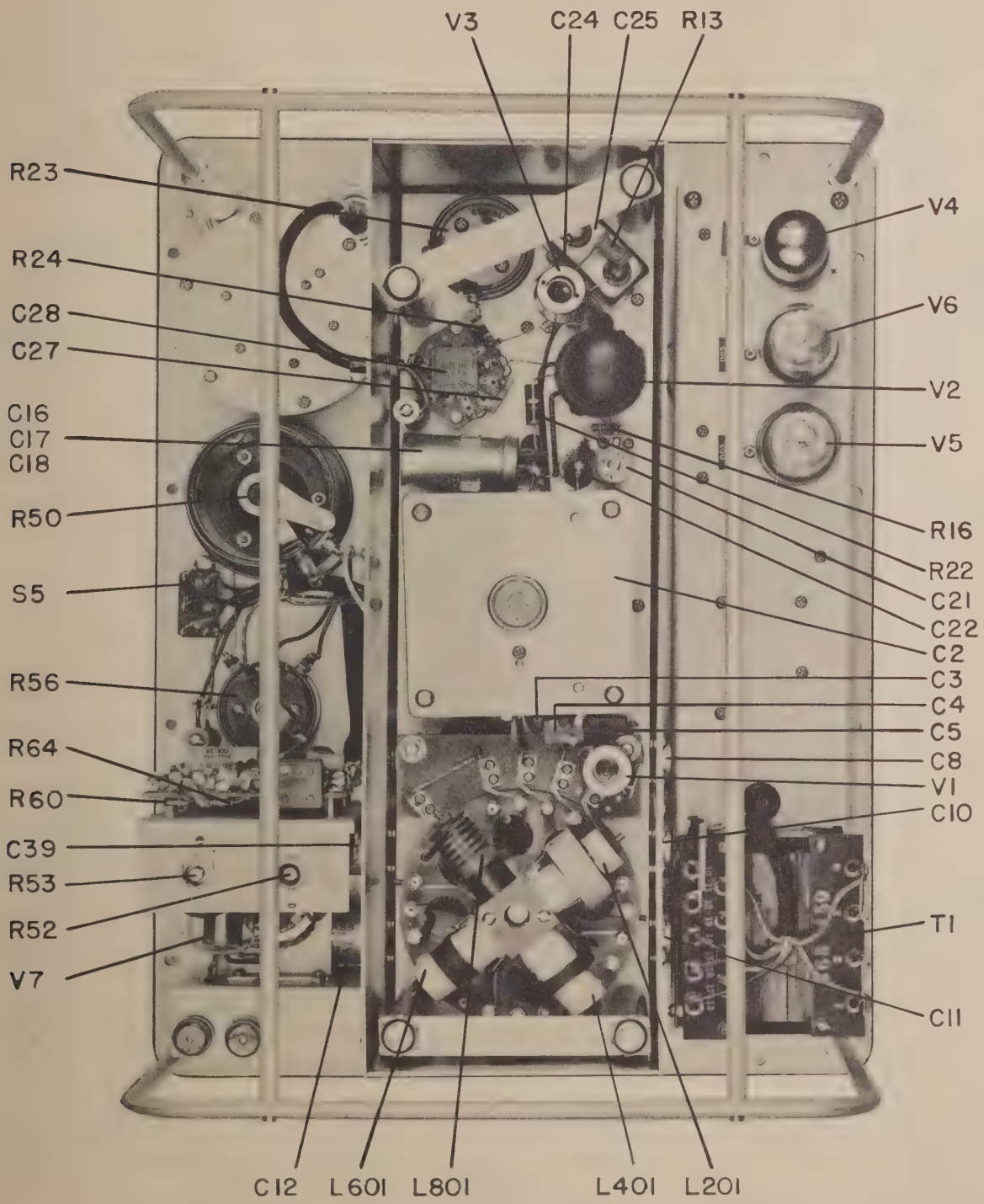
*Except for three lowest ranges which are 50k, 35k, and 25k for 5-15 kc, 15-50kc, and 50-150kc respectively.
**Anchor terminal.
Resistances in ohms unless otherwise specified by k (kilohms) or M (megohms).
Measurements made with 20,000-ohm/volt multimeter.
Connect a lead from pin 5 of V5 to ground when checking resistances.
Make all measurements from tube socket pins to ground, with tubes removed.

SWITCH POSITIONS

FREQ RANGE - 150-500 kc	METER - MODULATION
MODULATION - 400∼	OUTPUT - ATTEN
MODULATION - full clockwise	Output Pot. - set to zero
CARRIER - full clockwise	MULTIPLIER - 100mv



Front View of Oscillator Shelf showing Cable for Servicing.



Rear Interior View with Oscillator Shield Cover off.

PARTS LIST

Resistors

R2	47	K	±10%	REC-30BF
R3	300		±5%	REC-20BF
R4	100	K	±10%	REC-20BF
R6	270		±10%	REC-20BF
R7	270		±10%	REC-20BF
R8	270		±10%	REC-20BF
R9	560		±10%	REC-20BF
R10	33	K	±10%	REC-20BF
R11	270		±10%	REC-20BF
R12	1	K		POSW-3
R13	8.25	K	±1%	REF-70
R14	5.1	K	±5%	REC-20BF
R15	56	K	±10%	REC-20BF
R16	750	K	±5%	REC-20BF
R17	30		±5%	REC-30BF
R18	100		±10%	POSC-25
R19	560	K	±10%	REC-20BF
R20	82		±5%	REC-20BF
R21	5.6	K	±1%	REF-65
R22	1	K	±10%	REC-41BF
R23	50			P432-305-2
R24	350		±1/2%	1001-29
R25	95			P432-304
R30	95		±1/2%	1001-201-3
R31	11.68		±1/2%	1001-201-3
R32	99		±1/2%	1001-201-2
R33	12.22		±1/2%	1001-201-2
R34	99		±1/2%	1001-201-2
R35	12.22		±1/2%	1001-201-2
R36	99		±1/2%	1001-201-2
R37	12.22		±1/2%	1001-201-2
R38	99		±1/2%	1001-201-1
R39	11.0		±1/2%	1001-201-1
R41	15		±10%	REW-3
R42	6.2	K	±5%	REC-20BF
R43	560		±10%	REC-20BF
R44	560		±10%	REC-20BF
R45	1.6	K	±10%	REPO-20P
R46	1.6	K	±10%	REPO-20P
R47	1.5	K	±10%	REPO-20P
R48	1	K	±10%	REPO-20P
R49	100		±10%	REC-20BF
R50	30	K	±10%	371-416
R51	20	K	±10%	REPO-16
R52	5	K		POSW-3
R53	20	K		POSC-11
R54	22	K	±5%	REC-20BF
R55	22	K	±5%	REC-20BF
R56	20	K		301-431
R57	10	K	±10%	REC-20BF
R60	2.2	M	±10%	REC-20BF
R61	27	K	±10%	REC-30BF
R62	1	M	±10%	REC-20BF
R63	1	K	±10%	REC-20BF
R64	680	K	±10%	REC-20BF
R65	107	K	±1%	REF-70
R66	517	K	±1/2%	REF-70
R67	517	K	±1/2%	REF-70
R68	100		±10%	REC-20BF
R69	2.4	K	±5%	REC-20BF
R70	120	K	±10%	REC-20BF
R101	47	K	±10%	REC-20BF
R201	33	K	±10%	REC-20BF
R301	24	K	±5%	REC-20BF

Capacitors

C2	820	μμf		848-404
C3	0.002	μf	±10%	COM-30B
C4	100	μμf	±10%	COM-20B
C5	0.01	μf	±10%	COM-35B
C6	0.5	μf	+20%,-10%	COU-17
C7	0.5	μf	+20%,-10%	COU-17
C8	0.5	μf	+20%,-10%	COU-17
C9	0.5	μf	+20%,-10%	COU-17
C10	0.5	μf	+20%,-10%	COU-17
C11	0.5	μf	+20%,-10%	COU-17
C12	0.5	μf	+20%,-10%	COU-17
C14	400	μμf		Built in
C15	400	μμf		Built in
C16	10	μf	+70%,-10%	COEB-4
C17	10	μf	+70%,-10%	COEB-4
C18	5	μf	+70%,-10%	COEB-4
C20	200	μμf	±10%	COU-8-2
C21	1.5-7	μμf		COT-17
C22	0.47	μf	±10%	COL-71
C23	200	μf	±10%	COE-15
C24	500	μμf	50 DCWV	COM-20B
C25	0.05	μf	±10%	COL-1
C27	500	μμf	±10%	COM-20B
C28	0.01	μf	±10%	COM-35B
C30	0.01	μf	+20%,-10%	COU-16
C31	0.01	μf	+20%,-10%	COU-16
C33	3000	μf	+100%,-10%	COE-9
C34	20	μf	+50%,-10%	COEB-25
C35	20	μf	+50%,-10%	COEB-25
C36	20	μf	+50%,-10%	COEB-25
C37	20	μf	+50%,-10%	COEB-25
C38	20	μf	+50%,-10%	COE-5
C39	0.5	μf	±10%	COL-4
C40	200	μμf	±10%	COM-20B
C41	0.001	μf	±10%	COM-20B
C42	0.02	μf	±10%	COL-33
C43	0.001	μf	±1%	COM-30C
C44	0.001	μf	±1%	COM-30C
C45	0.002	μf	±1%	COM-30C
C46	0.02	μf	±10%	COL-33
C47	200	μμf	±10%	COM-20B
C48	200	μμf	±10%	COM-20B
C101	5-20	μμf		COT-18
C201	7-45	μμf		COT-12
C301	7-45	μμf		COT-12
C302	125	μμf	±10%	COM-20B
C401	7-45	μμf		COT-12
C501	7-45	μμf		COT-12
C601	7-45	μμf		COT-12
C701	7-45	μμf		COT-12
C801	5-20	μμf		COT-18

Switches

S1	8 Position Freq. Selector	1001-305
S2	4 Position	SWRW-37
S3	6 Position Att. Switch	1001-39
S4	D.P.S.T. (mounted on S6)	
S5	D.P.D.T. SWT-335	
S6	4 Position (with S4)	SWRW-36

Fuses

F1	0.8 amp.	3AG	Slo-Blow	For 115
F2	0.8 amp.	3AG	Slo-Blow	operatio
F1	0.4 amp.	3AG	Slo-Blow	For 230
F2	0.4 amp.	3AG	Slo-Blow	operatio

Inductors

L1	250	mh	GR	119-30
L3	60	mh	GR	1001-28
L4	1.0-1.6	μh	GR	CHA-59-1
L101	1.335	mh	GR	1001-222
L201	137	mh	GR	1001-205-2
L301	13.35	mh	GR	1001-205-3
L401	1.37	μh	GR	1001-205-4
L501	133.5	μh	GR	1001-205-5
L601	13.5	μh	GR	1001-206
L701	1.1	μh	GR	1001-207
L801	0.13	μh	GR	1001-208

Tubes

V1	6C4
V2	6L6/1614
V3	6AL5
V4	5Y3-GT
V5	0C3
V6	0C3
V7	6SN7-GT

Miscellaneous

J1	Jack	1001-323
J2	Jack	874-4533
J3	Jack	1001-313
PL1	Plug	ZCDPP-10
PL2	Plug	1001-219
PL3	Plug	1001-34
D1	Diode	1N34-AS
D2	Diode	1N34-AS
D3	Diode	1N3028
T1	Transformer	365-459
M1	Meter (200μa)	MEDS-31
P1	Pilot Light	2LAP-939 Mazda #44
SO1	Socket	1001-218

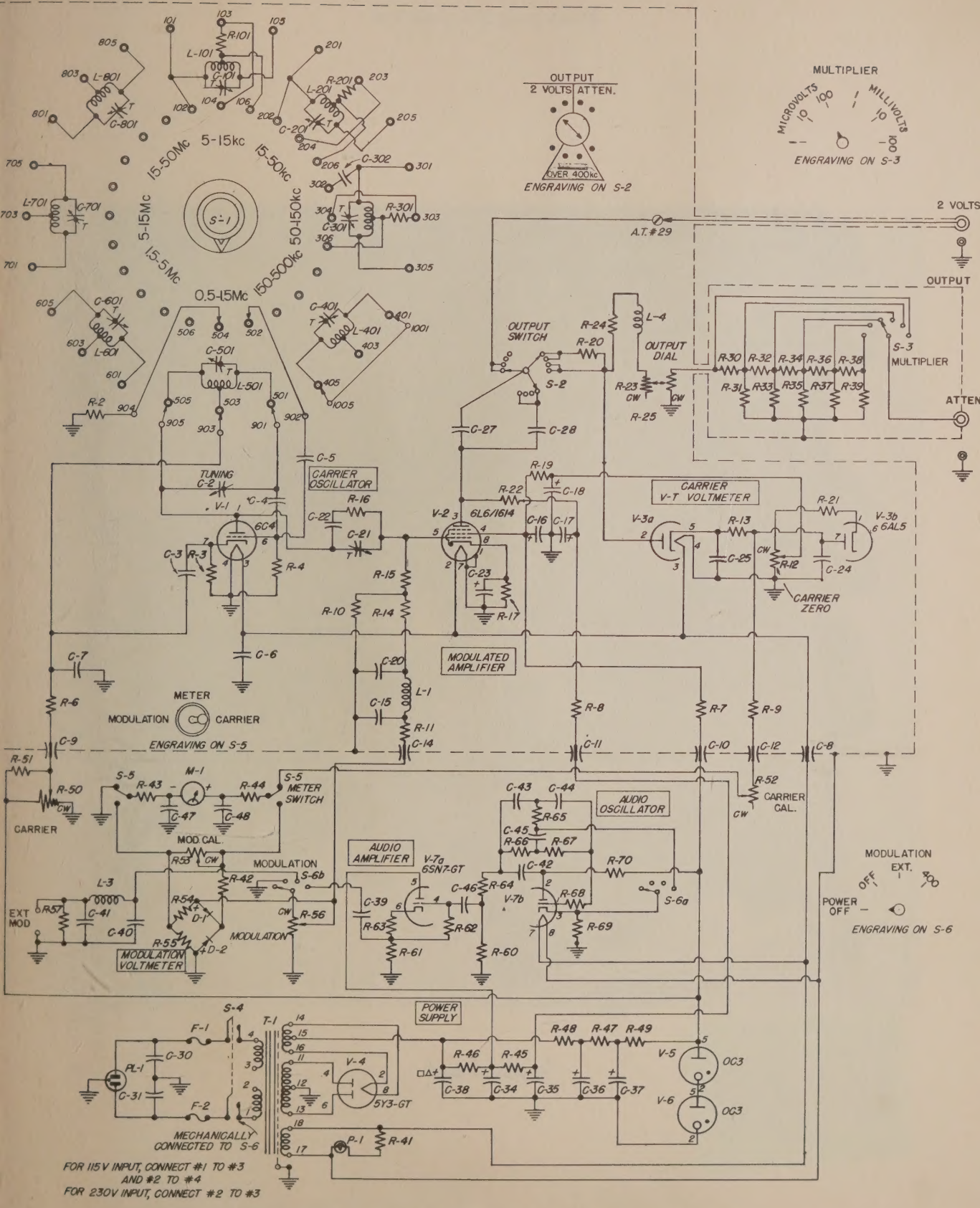
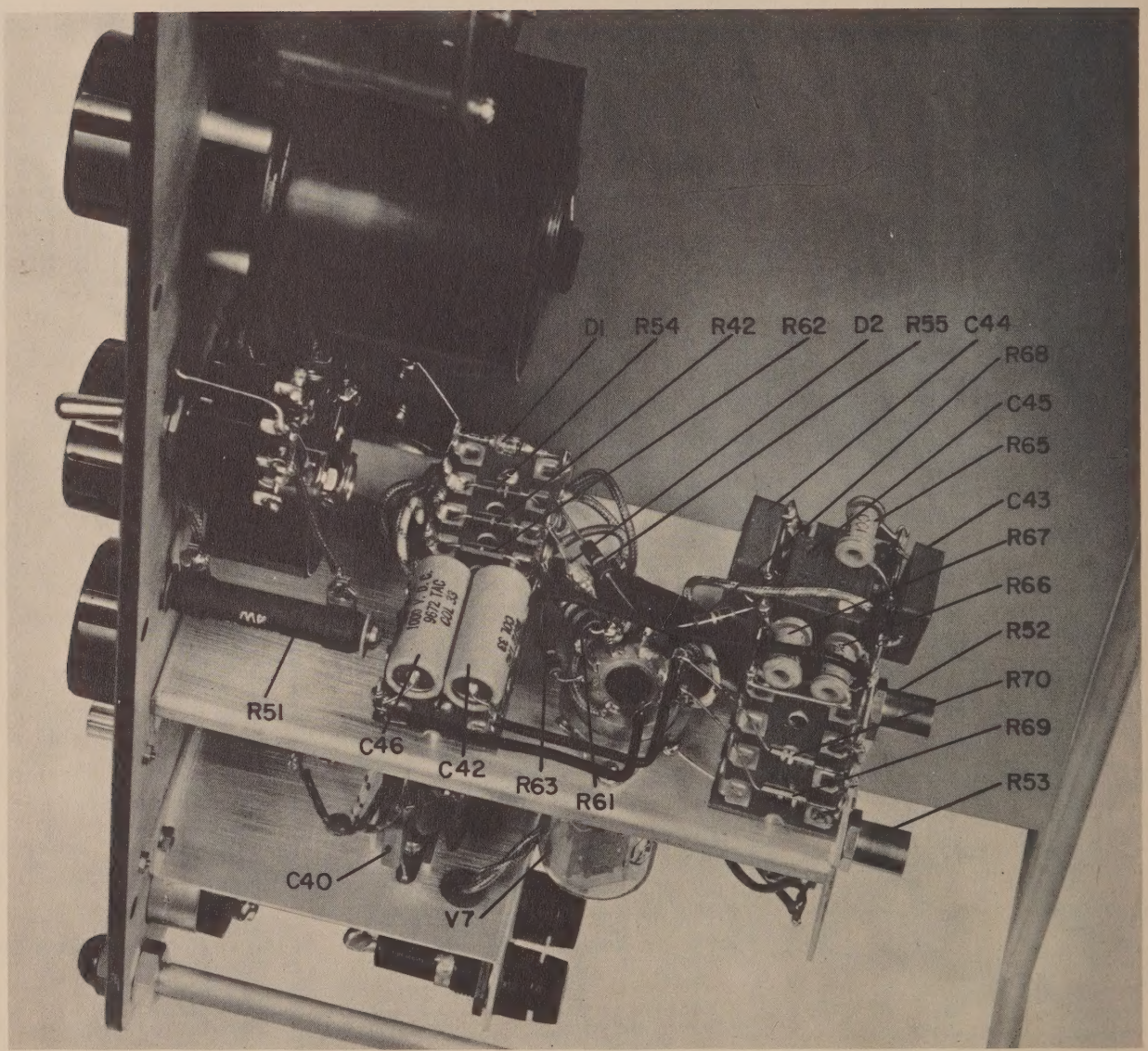


Figure 3. Wiring Diagram for Type 1001-A Standard Signal Generator



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